

## Motivation: Urban heterogeneity

A worldwide growing urban population puts cities are under increasing pressure from resource scarcity, air pollution and climate change. These challenges demand a better understanding of the local climate effects of urban environments.



Figure 2: Urban heterogeneity in the city of London. ©User:Colin and Kim Hansen/Wikimedia Commons

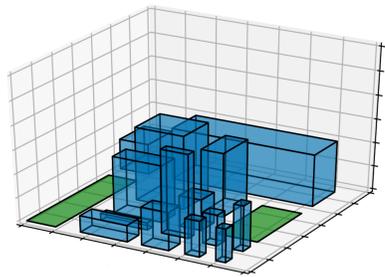


Figure 1: Generating an urban landscape model with building blocks and green space.

One complexity of modelling urban climate comes from the heterogeneity of urban areas. Densely mixed building units of various sizes and shapes, complex road networks, paved surfaces, water and urban vegetation all interact with each other and the atmosphere.

## Dales-Urban LES model

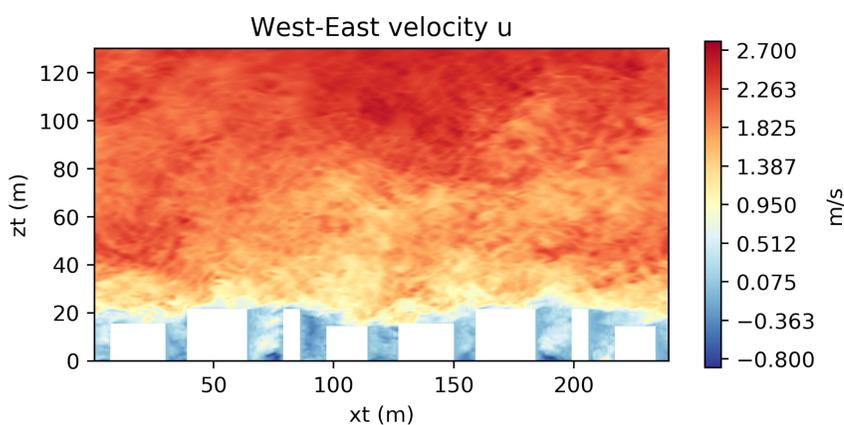


Figure 3: Instantaneous streamwise velocity field with heterogeneous surface.

Dales-Urban is a Large-Eddy Simulation (LES) model that resolves the turbulent urban flow field at resolutions of 1 m and 0.5 s.

## Momentum balance of the governing equation

Decomposition of variables into space-time mean  $\langle \cdot \rangle$ , space variations of time mean  $\bar{\cdot}$  and fluctuations  $'$ , and averaging the governing Navier-Stokes equations in horizontal space  $\langle \cdot \rangle$ , and time  $\bar{\cdot}$  yields the vertical momentum balance:

$$\frac{\partial}{\partial z} \left( \underbrace{\langle \bar{w}'u' \rangle}_{\text{turbulent flux}} + \underbrace{\langle \bar{w}''u'' \rangle}_{\text{dispersive flux}} - \underbrace{\nu \frac{\partial \langle \bar{u} \rangle}{\partial z}}_{\text{viscous flux}} \right) + \underbrace{\frac{1}{\rho A} \int_{\partial \Omega_{xy}} \bar{p}'' n dS}_{\text{form drag}} - \underbrace{\frac{\nu}{A} \int_{\partial \Omega_{xy}} \frac{\partial \bar{u}_i''}{\partial n} dS}_{\text{skin drag}} = \underbrace{\langle \bar{F} \rangle}_{\text{pressure forcing}}$$

## Vertical transport: heterogeneity increases momentum sinks

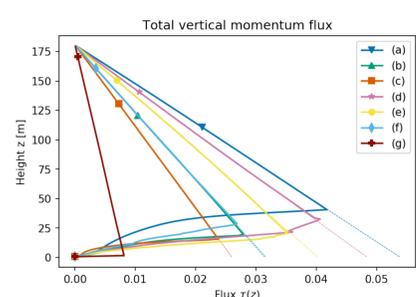


Figure 4: Total vertical transport of horizontal momentum  $\tau$ , including extrapolated forcing  $\hat{F}$  to the domain bottom surface.

canopy, and more heterogeneous layouts tend to have larger momentum sinks. The integrated drag term plays an important role as momentum sink and correlates to maximum building height  $z_{\max}$  and average height plus deviation  $z_H + \sigma_H$ , respectively. Turbulent fluxes are the main contributor to the vertical momentum transport, dispersive fluxes contribute within and close above the urban canopy.

The total vertical momentum flux describes the vertical movement in the flow. The rate of downwards momentum transport is highest around the top of the urban

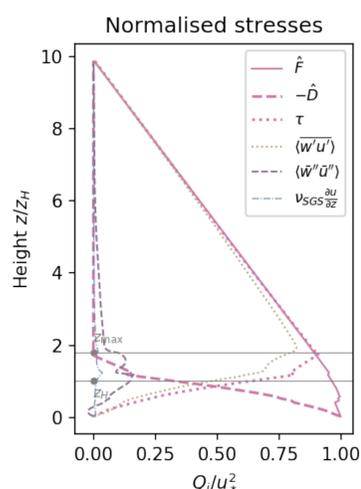


Figure 5: Contributions from the integrated terms of the momentum balance equation to vertical momentum transport.

## Simulation setups with varying heterogeneity

Simulations of different urban landscapes (a to f), which share a similar building density  $\lambda_p$  and wind-facing surface  $\lambda_f$ . The landscapes vary in street geometry, building plan area and building height. A reference simulation (g) contains no urban elements.

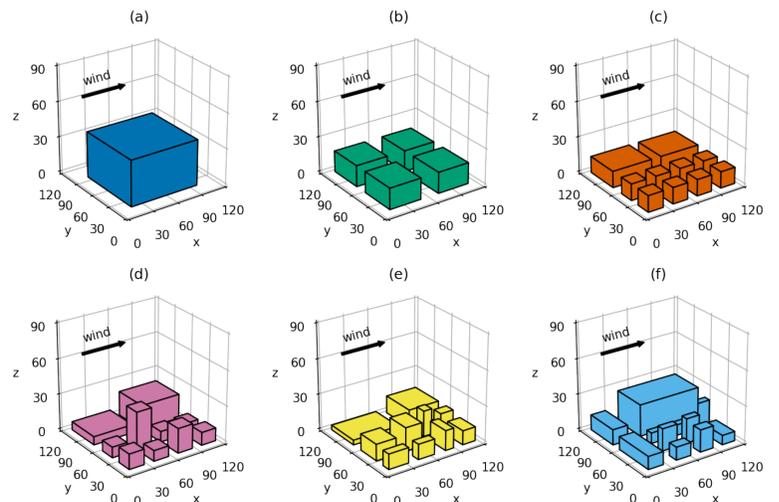


Figure 6: Block layouts for six simulations (a) to (f) with varying heterogeneity.

	$\lambda_p$	$\lambda_f$	$n_b$	$z_{\max}$	$z_H$	$\sigma_H$	H/W	W/R
(a)	0.46	0.22	1	39 m	39 m	0 m	1.03	0.32
(b)	0.45	0.22	4	18 m	18 m	0 m	0.82	0.37
(c)	0.46	0.22	10	14 m	14 m	0 m	1.17	0.33
(d)	0.46	0.22	10	32 m	18.07 m	8.43 m	1.18	0.33
(e)	0.46	0.22	10	22 m	15.57 m	4.04 m	1.15	0.35
(f)	0.45	0.24	10	27 m	18.27 m	7.16 m	1.25	0.33

Table 1: Block statistics: plan area fraction  $\lambda_p$ , frontal aspect ratio  $\lambda_f$ , number of blocks  $n_b$ , maximum block height  $z_{\max}$ , weighted average block height  $z_H$ , block height standard deviation  $\sigma_H$ , block height to canyon width average H/W, canyon to combined block and canyon width average W/R.

## Mean flow: distinct flow profiles with heterogeneity

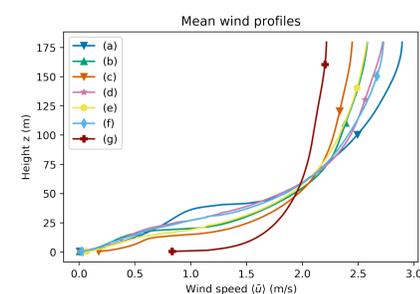


Figure 7: Averaged vertical wind velocity  $\langle \bar{u} \rangle$  of simulations (a) to (g). The volume-averaged flow rate of all simulations is  $u = 2$  m/s.

Building blocks obstruct the mean flow and a logarithmic boundary layer profile develops above the urban canopies. The flat surface (g) shows a typical boundary-layer profile. Setups (a) to (c) with homogeneous building heights show a clear distinction between canopy flow and free flow. Velocity profiles changes from concave (within) to convex (above canopy). Setups (d) to (f) with heterogeneous building heights have a gradual regime change and lack a clear separation of above- and within-canopy flow.

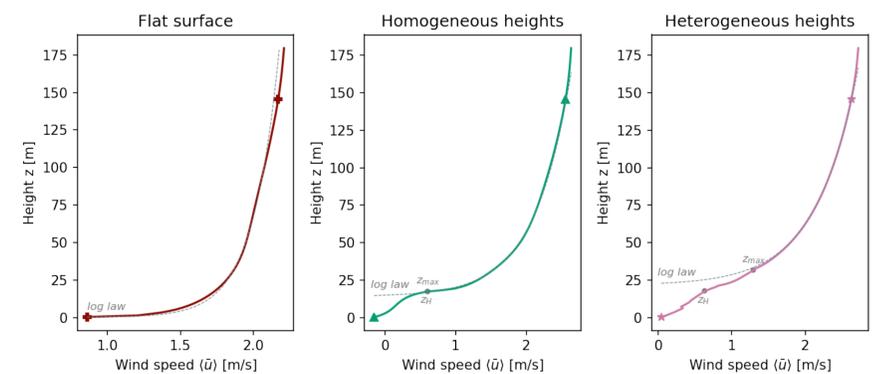


Figure 8: Mean wind flow regimes for flat surface, homogeneous and heterogeneous building heights.

## Conclusions

- Heterogeneous building layouts produce distinct flow regimes and vertical momentum flux profiles, parameters  $\lambda_p$  and  $\lambda_f$  are not sufficient to describe them.
- Greater momentum sinks result from larger turbulence-related momentum fluxes and building-induced drag. Heterogeneity parameters such as  $z_{\max}$ ,  $z_H$  and  $\sigma_H$  are predictors for an increased rate of momentum loss within urban canopies.

## References

1. Heus, T. *et al.* Formulation of the Dutch Atmospheric Large-Eddy Simulation (DALES) and overview of its applications. *Geoscientific Model Development* 3, 415–444 (2010).
2. Suter, I. L. *Simulating the impact of blue-green infrastructure on the microclimate of urban areas.* PhD thesis (Imperial College London, 2018).
3. Tomas, J. M. *et al.* Stable Stratification Effects on Flow and Pollutant Dispersion in Boundary Layers Entering a Generic Urban Environment. *Boundary-Layer Meteorology* 159, 221–239 (2016).